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Open-Source Antenna Pattern Measurement System SDR-based Student Research and Development

Abstract

Weber State University (WSU) has developed an 'open-source' antenna-pattern measurement system physically comprised of software-defined radios (SDRs) and 3-D printed hardware. The present WSU 'open-source' prototype integrates Python, GNU Radio Companion, and Linux on a single laptop PC. Multiple student projects have investigated methods to improve measurement fidelity in non-optimal environments. For example, excellent agreement between measured and simulated radiation patterns has been obtained using coherent AM detection. The following paper summarizes the development of the current system and presents results from student research.

1. Introduction

1.1. Background

Electrical Engineering faculty at Weber State University (WSU) have pursued software-defined-radio (SDR) applications to expand RF measurement capabilities for education and applied research. Examples of open-source SDR instrumentation developed for RF measurements include periodic and random Jitter (G. Anthonys & Streeter, 2019), RFID system performance (D. DeDonno, January 2013), and array localization algorithms (V. Goverdosvsky, July 2016). Sections 2 describe the development of an SDR-based antenna radiation pattern measurement system presented at the AMTA 2020 conference (C.W. Hearn, 2020). Section 2.6 summarizes the analysis of two modulation methods in a non-anechoic environment (Hansen, 2020). The antenna pattern measurement system developed at WSU was inspired by the published work of Picco and Martin (V. Picco, Dec 2011). Their practical system utilized commerciallyavailable 2.4 GHz wireless routers. Open-source (DD-WRT) software replaced the original firmware. An estimate of the received field strength was obtained from the (DD-WRT accessible) received signal strength indicator (RSSI) measured between routers. Antenna position control and RF signal measurement were realized using National Instruments LabVIEW (https://www.ni.com/en us/shop/labview.html). The Picco and Martin (P&M) prototype was developed and results were published in 2011. Since the publication of their results, softwaredefined-radios (SDRs) have become economically viable for student projects. In addition, the tremendous growth of three-dimensional printer technology has made available hardware well-suited for integration to a pattern measurement system. The GNU Radio software library (https://wiki.gnuradio.org/index.php/Mainpage) was chosen for the WSU project to maintain the flexibility of LabVIEW with commercial software fees. GNU Radio Companion is a Linux-based open-source software platform for communication and signal processing that is wellsuited for student-initiated code development. Position control is achieved using an Arduino microcontroller with open-source software developed for 3-D printer systems (https://grbl controller.software.informer.com/3.6/.). Lowcost, commercially-available three-dimensional printer hardware (e.g. gears, synchronous belts) and software are utilized for position-control. The following sections describe the development and current research of an opensource antenna pattern measurement system. A summary of current research describes the assessment of a coherent modulation method utilized to reduce measurement noise interference in non-anechoic environments.

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1.2. Feedback from Paper Submission

Complete developments of pattern, directivity, and gain discussed in the following sections are available in numerous texts. Two popular examples include (W. L. Stutzman, 1998) and (Balanis, 1997). An antenna pattern is a graphical representation of the normalized (electric) field magnitude at a fixed distance from the antenna as a function of direction. (1)

$$F(\Theta, \Phi) = \frac{E(\Theta, \Phi)}{E_{MAX}}$$

Normalized directivity is the radiated power density relative to the measured maximum power density. Normalized Directivity and Gain are related to the square of the antenna pattern. (2)

$$F(\Theta, \Phi)|^2 = \frac{D(\Theta, \Phi)}{\Phi} = \frac{G(\Theta, \Phi)}{\Phi}$$

$$|F(\Theta, \Phi)|^{2} = \frac{D(\Theta, \Psi)}{D_{MAX}} = \frac{G(\Theta, \Psi)}{G_{MAX}}$$
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Preliminary work. Under review by the GNU Radio Conference (GRCON). Do not distribute.

110 An approximation of the gain from the measured pattern of 111 a lossless antenna may be determined by scaling the mea-112 sured data to a calculated gain. (3)

$$G(\Theta, \Phi) \approx G_{Total} \cdot |F(\Theta, \Phi)|^2$$

A Method of Moments commercial software (e.g. FEKO) may be used to model the prototype and calculate maximum Gain values. Comparisons of measured patterns to simulation are straightforward once the measured pattern data is normalized and scaled to the calculated maximum gain. The method described is limited to a qualitative check, but it would be a relevant demonstration of validation in an educational setting.

1.3. Linksys Prototype

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126 Two WSU undergraduates reconstructed the P&M system 127 as part of a senior capstone project. The reconstructed sys-128 tem utilized readily-available Linksys routers connected to 129 the reference antenna (SOURCE) and the antenna-under-130 test (AUT). Open-source firmware (DD-WRT) was loaded 131 on the routers to access the RSSI level versus position. Na-132 tional Instruments LabVIEW software controlled two step-133 per motors for elevation and azimuth orientation of the 134 AUT. The senior project obtained coarse pattern measure-135 ments of a test antenna, however difficulties mentioned in 136 the original article reappeared with the WSU recreation of 137 the P&M prototype.

¹³⁹140**2. Open-Source SDR Prototype**

141 **2.1. First SDR Prototype**

142 A second antenna pattern measurement system prototype 143 was developed with modifications focused primarily on ad-144 dressing mechanical challenges (e.g. slippage, position 145 control) and single frequency operation. A photograph of the current prototype is shown in Figure 1. The mechani-147 cal system was redesigned with a focus on the use of PVC 148 components and synchronous-belt hardware. Design and 149 fabrication of the rapid-prototype-material (RPM) parts are 150 discussed in Section 2.3. The second system consisted of 151 two SDRs, two stepper motors, and one Arduino Uno to 152 control the stepper motor drive board. A block diagram of 153 the complete system is shown in Figure 2. One computer 154 was dedicated to operate the control software with a user 155 interface. A summary of the 2nd prototype modifications 156 include: 157

- Open source motor control
- GRBL on Arduino, easy to modify/configure
- Synchronous (toothed) belts/pulleys
- Hack RF software-defined radios

- 30 MHz-6 GHz potential frequency range
- GNU Radio Software control of SDRs

Modifications chosen for the second prototype increase cost and system complexity. Potential increases in capability and measurement accuracy were justification for the design modifications.

2.2. Position and Data Acquisition Control

An Arduino microcontroller with a commercially-available motor-driver shield establishes position control for the AUT. An external power supply provides 12 Volts DC and up to a maximum 30 Amps pulses to drive the stepper motors. Control of the motors is established through a series of GRBL 'G-code' commands over the virtual serial port provided by Arduino. G-code commands are sent to the GRBL motor control firmware to control position, speed, and direction of the stepper motors during measurements. GRBL is an open-source firmware for CNC machines and 3D printers. G-code is used by hobbyists for 3-D printing as a standard for directing spindle/nozzle movement.



Figure 1. Antenna Pattern measurement system. Emphasis was placed on use of commercial PVC material with 3-D printer hardware including synchronous belts and gears



Figure 2. Block diagram of Antenna Pattern Measurement system.

2.3. Mechanical Design

Mechanical modifications to the P&M design proceeded with the design goal to utilize commercial off-the-shelf (COTS) components when possible. Custom parts were prototyped on-site. Design challenges related to the Antenna Pattern Measurement System included the multi-axis movement requirements, control of mast motion, and low conductivity of the structure and motors to minimize scattering/interference with the antenna signal reception. The azimuth and elevation control stepper motors were chosen to minimize EMI with the measured signal. Synchronous drive belts used in commercial 3-D printers were incorporated to rotate the AUT mast about two axes of motion. Future measurement prototypes will include bearings constructed of non-conductive polymer material were also procured and included in the drive system. The primary structure was constructed of commercially available plastics, including PVC pipe to minimize the costs. Custom parts were designed and fabricated at Weber State University. Examples include the synchronous belt sprockets, and mounting brackets. Images of the custom designed parts used in the Antenna Pattern Measurement System assembly are presented in Figure 3. SolidWorks 3D CAD software was utilized in the design process to verify functionality, clearances, as well as range of motion. The mechanical design also included the mounting and packaging of the associated electronics, stepper motors, and power supply.





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Figure 3. Antenna Pattern Measurement System Prototype Part CAD Models.

2.4. Measured Results

Prototypes of three antennas were constructed to evaluate an antenna design and development process for undergraduate students. It is anticipated future student-built prototypes will be designed for Wi-Fi band $(f \approx 2.4 GHz)$ with a free-space wavelength of approximately $\lambda \approx 12.5 cm$. Models were constructed using commercial Method-of-Moments software (FEKO) for comparison. Measured Radiation pattern data was scaled to the simulated Gain values (GTOT) for a quarter-wave monopole over a finite ground plane, a Yagi-Uda directional antenna, and an air-backed circular micro-strip patch antenna. Discussion of the validation step and presentation of results are available.(Hearn, 2020)

2.5. Noise-Subtraction versus Coherent AM

A Noise-subtraction method of measuring received signal strength was implemented with the first WSU prototype. Statistical characterization of noise power may be investigated in the future, but a straightforward noise-subtraction algorithm Intro-define noise-subtraction method as state it is the original data acquisition algorithm for the WSU prototype. The 'noise subtraction' method of measuring signal strength transmits and measures a received uniform noise signal. At each position, an ambient-noise and signal+ambient-noise are recorded. The ambient-noise measurement is subtracted from the signal+noise measurement. An example of a principal plane pattern (in linear format) of the 2.4 GHz Yagi prototype is shown in Figure 4. Coherent Amplitude Modulation (Double-Sideband-Suppressed Carrier - DSB-SC-AM) is the linearmodulation method integrated to the WSU antenna pattern measurement system. The close proximity of the source



Figure 4. Example of 2.4 GHz Yagi prototype measured pattern using noise reduction method.

The coherent DSB-SC AM system was developed based on the work of Saraswati, Asuti, and Mishra [14]. A DSB-SC AM transmitter and receiver, shown in Figures 5 and 6 respectively, were developed using GNU radio software and the same Hack RF One SDRs described in Section III. The osmocom source block receives the signal measured by the SDR receiver. The signal is then multiplied by the carrier signal. The carrier signal is the same 2.4 GHz sinusoid used in transmitter. The multiplication shifts the frequency to baseband. For long-range communication receivers us-ing coherent detection, a Costas loop is used to lock the phase of the DSB-SC AM signal with the phase of a local oscillator set to the carrier frequency (S. B. Saraswati & Mishra, 2016). The carrier signal at the SDR transmitter



Figure 5. DSB-SC AM Transmitter Flow Chart.

and the SDR receiver were synchronized by connecting the clock signal of the SDR transmitter to the clock signal of



Figure 6. DSB-SC AM Receiver Flow Chart.

the SDR receiver. Figure 7 is a comparison plot (linear format) of a principal plane plots of normalized patterns of the 2.4 GHz Yagi prototype using the two methods. The noise-subtraction method shown in Figure 4 is compared to the coherent-AM method described.

2.6. Comparison of Modulation Methods

Antenna measurements in an 'ideal' (anechoic) environment using measurement-grade RF hardware would be the first choice for an accurate quantitative comparison of the two modulation methods. Research-grade patterns could be used as a basis for quantitative comparison. Limited resources required an alternative approach (J.McCormick & Parini, Dec 2011). A repeatability campaign with multiple pattern measurements for the three prototypes under similar conditions was completed for the analysis. Twelve antenna pattern measurements were taken of each of the three antennas using the noise subtraction method. Twelve additional measurements of each antenna were completed using the noise coherent DSB-SC AM method. A small sample size of 12 was chosen because of the long length of time required in obtaining each antenna pattern measurements. Following an approach described by (Stark & Woods, 1994), a margin of error, at each angular position was calculated using equation for both the noise subtraction method and the coherent DSB-SC AM method.

$$\epsilon = t \frac{\sigma}{\sqrt{n}}$$

In the equation above σ is the standard deviation of the n=12 data points at one specific angular position. A t-distribution table was used to select values of t for the above equation to give a margin of error with a 95% confidence.



Figure 7. Measured principal plane pattern boresight ($\Theta = 90^{\circ}, 180^{\circ} < \Phi < 180^{\circ}$) of the Yagi antenna prototype. Both the Coherent DSB-SC AM and Noise Subtraction methods are shown for comparison.



Figure 8. Mast head created from 3-D printed materials

3. Upgrades

3.1. Hardware

The latest antenna pattern measurement system was developed replacing the older PVC components with 3-D printed parts modeled in Solid-works. The new design was created in order to make a more mobile system. The more mobile system allows students to test antennas in multiple noisy environments. As well as, the system is better suited for outreach and collaboration events.

3.2. Software

The software of the system was upgraded through student efforts and research. The list of upgraded software include:

- Python 3.6.5 Python 3.9
- GNU Radio 3.7.13.4 3.9.2.0
- Linux 4.19 Debian Bullseye

One major point of research was the transmitter gain on the newest systems distorted directional antennas. In previous systems the RF and IF gain were set to the max of 14 and 47 respectively. When ran on the newer laptops the main lobe of directional antennas were clipped off, exaggerating side lobes. The gain was modified in the python code down to 0 and the expected patterns were once again recorded.

3.3. Platform

Raspberry Pi's run on an offshoot of Linux Debian called Raspbian or Raspberry PI OS. An SD card is programmed with the latest Raspbian software. The dependencies and python version is updated to match former PC tests. The first antenna tests are run on a Raspberry Pi 3. The antennas used are a quarter wave mono-pole and a patch antenna with no ground plane. A second set of measurements are recorded on a Raspberry Pi 4. The raspberry Pi 3 had significant noise in the measured data. Figure 9 shows a mono-pole antenna pattern measured with both the Raspberry Pi 3 and Raspberry Pi 4. Figure 10 is a similar measurement with a patch antenna. The controllable variables were kept constant in every measurement. The same antenna, SDR, and distance between antennas were used in each test. The same SD card was swapped back and forth between the PI 3 and PI 4 to create an exact match of the recorded software. "DRI2 Failed to authenticate" errors plagued the PI 3 test as well. The only working solution was to reboot the PI 3 pointing to a memory issue. However, more research would be needed to narrow down the exact cause. The PI 3 was concluded to be insufficient indata measurement and analysis compared to the PI 4.



will continue to be an educational resource suitable for introductory antenna characterization. Applied research areas will focus on the optimization of antenna pattern measurements in non-anechoic environments. The open-source antenna pattern measurement system has also created collaboration opportunities with other universities.

Figure 9. Raspberry Pi 3 vs 4 Mono-pole Antenna.



Figure 10. Raspberry Pi 3 vs 4 Patch Antenna.

4. Conclusions and Future Work

A low-cost antenna pattern measurement system based upon the Picco and Martin concept was modified to incorporate software-defined radios and commercial hardware. Additional parts were constructed using 3-D printer technology. Comparisons of simulated and measured gain patterns for three lossless antennas are presented. A qualitative comparison of the two modulation methods indicates the coherent modulation technique results in smoother antenna pattern measurements. The system has undergone several upgrades from software to hardware through student efforts. The automated antenna measurement system

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References

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- Balanis, C. A. Antenna Theory- Analysis and Design. Wiley Sons, 2nd edition, 1997.
- C.W. Hearn, D. Newton, et al. Open-source antenna pattern measurement system. Technical report, Antenna Measurement Techniques Association Conference (AMTA), 2020.
- 676 D. DeDonno, F. Ricciato, L. Tarricone. Listening to tags: 677 Uplink rfid measurements with an open-source software-678 defined radio tool. IEEE Trans. Instrum. Meas., 62(1): 679 109-118, January 2013. 680
- G. Anthonys, M.J. Cree and Streeter, L. Jitter measure-681 ment in digital signals by using software defined radio 682 683 technology. IEEE Int'l Instrumentation and Measurement Technology Conference (I2MTC), 2019. 684
- 685 Hansen, T. Open-Source Antenna Pattern Measurement 686 Systems Using Coherent DSB-SC Amplitude Modula-687 tion. PhD thesis, Weber State University, 2020. 688
- 689 Hearn, C.W. Open-source antenna pattern validation using 690 feko. Technical report, Applied Computational Electro-691 magnetics Society (ACES), 2020. 692
- 693 https://grbl controller.software.informer.com/3.6/. Grbl 694 controller. get the software safely and easily. 695
- 696 https://wiki.gnuradio.org/index.php/Mainpage.Gnuradio. 697
- 698 https://www.ni.com/en us/shop/labview.html. What is lab-699 view? graphical programming for test amp; measurement. 700
- J.McCormick, S. F. Gregson and Parini, C. G. Quantitative measures of comparison between antenna pattern data sets. 703 IEEE Proceedings - Microwaves, Antennas and Propagation, 152(6):539-550, Dec 2011. 704
- 705 S. B. Saraswati, M. G. Asuti and Mishra, A. Dsb-sc am based 706 software defined radio(sdr) design. 2016 IEEE Interna-707 tional Conference on Recent Trends in Electronics, Infor-708 mation Communication Technology (RTEICT), pp. 1356-709 1360, 2016. 710
- Stark, H. and Woods, J. W. Probability, random processes and 712 estimation theory for engineers. Englewood Cliffs, pp. 276, 713 1994. 714

Jury 2010. 719 V. Picco, K. Martin. An automated antenna measurement system utilizing wi-fi hardware. <i>IEEE Antennas Propagation Magazine</i> , 53:179–183, Dec 2011. 720 W. L. Stutzman, G.A. Thiele. Antenna Theory and Design. 724 Wiley Sons, 2nd edition, 1998. 725 728 728 729 730 730 731 731 732 732 733 733 734 734 735 735 736 736 737 737 738 738 739 739 740 741 742 742 743 743 744 744 745 745 746 746 747 747 748 748 745 749 740 741 742 744 745 745 746 746 747 747 748 748 746 749	radio testbed for rapid prototyping of localization algo- rithms. <i>IEEE Trans. Instrum. Meas.</i> , 65(7):1577–1584, July 2016	716 717 718
V. Picco, K. Martin. An automated antenna measurement system utilizing wi-fi hardware. IEEE Antennas Propagation Magazine, 53:179–183, Dec 2011. 721 W. L. Stutzman, G.A. Thiele. Antenna Theory and Design. Wiley Sons, 2nd edition, 1998. 723 728 726 729 720 720 722 721 722 722 723 Wiley Sons, 2nd edition, 1998. 726 720 723 723 724 724 725 725 726 726 727 728 726 729 730 730 730 731 732 732 730 733 734 734 734 735 736 736 737 737 738 738 739 739 740 741 743 742 743 743 744 744 745 745 756 750 757 <	July 2010.	710
tem utilizing wi-fi hardware. <i>IEEE Antennas Propagation</i> <i>Magazine</i> , 53:179–183, Dec 2011. W. L. Stutzman, G.A. Thiele. <i>Antenna Theory and Design</i> . Wiley Sons, 2nd edition, 1998. 726 727 788 729 730 730 731 733 734 734 735 736 737 738 739 740 741 742 743 744 745 746 746 747 755 756 757 758 758 756 757 758 756 757 758 756 757 758 756 757 758 757 758 756 757 758 757 758 759 759 759 759 759 759 759 759 759 759	V. Picco, K. Martin. An automated antenna measurement sys-	719
Magazine, 53:179–183, Dec 2011. 722 W. L. Stutzman, G.A. Thiele. Antenna Theory and Design. 723 Wiley Sons, 2nd edition, 1998. 725 726 726 727 728 729 730 731 732 732 733 733 734 734 735 735 736 736 737 737 738 738 739 744 744 745 736 736 737 737 738 738 739 744 744 745 746 746 747 748 749 749 750 751 752 753 756 756 756 757 758 758 756 759 760 761 762 763 764 764 765 765 756	tem utilizing wi-fi hardware. IEEE Antennas Propagation	720
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